

RECOVERY:
<i>\$</i> := ¤
$S := \frac{366915.5}{15288} \cdot \frac{lb}{15288} = 15288 \frac{lb}{15288}$
24 hr hr
T_{1} gru := 50 ° F = 510 B
$T_{MW} = 0.00 \ I = 0.00 \ R$
$FuelCost^{\&} = 1.33 \$
$Tueicosta := \frac{100000 \cdot Btu}{100000 \cdot Btu}$
E 152400 Btu
$FuelHV \coloneqq $
55
Waters :=
hr

Install Electronic Automatic Blowdown Control System:

<u>Existing Condition:</u> Currently blowdown is controlled manually and is blowdown to as high as 2800 TDS maximum. This is done by periodically blowing down boiler to 1840 average TDS. <u>Proposed Modification:</u> Install an electronic control system to automatically blowdown to more accurately track and maintain the setpoint of 2200 TDS. Savings would be in the ability to maintain the boiler TDS closer to the setpoint of 2200 and is estimated to provide an annual average increase in TDS of 360.

Existing Blowdown:

Blowdown Rate = (FxS)/(B-F)	$F \coloneqq 100$	$B_{Emist} \coloneqq 1840$	$S = 15288 - \frac{lb}{lb}$
F=Feed Water TDS (ppm)		Exist	hr
S=Steam generation rate (lb/hr)		BD	$F \cdot S$
B=Required boiler water TDS (ppm)			$B_{Exist} - F$

$$BD_{Exist} = 879 \frac{lb}{hr}$$
 $PercBD_{Exist} := \frac{BD_{Exist}}{S} = 5.75\%$

Proposed Blowdown:

Blowdown Rate = (FxS)/(B-F) F=Feed Water TDS (ppm)	F = 100	$B_{Prop} \coloneqq 2200 \qquad S = 15288 \frac{lb}{hr}$	
S=Steam generation rate (lb/hr)	$BD_{Prop} \coloneqq \frac{F \cdot S}{D}$	
B=Required boiler water TDS (p	opm)	$B_{Prop}-F$	
$BD_{Prop} = 728 \frac{lb}{hr}$ Pe	$ercBD_{Prop} \coloneqq \frac{BD_{Prop}}{S}$	=4.76%	



Enthalpy of saturated liquid at 150psig:

 $SH \coloneqq 338 \cdot \frac{Btu}{lb}$

 $EnergySavings_{Control} := \frac{(879 - 728)}{BE} \cdot \frac{lb}{hr} \cdot 339 \cdot \frac{Btu}{lb} \cdot HR$

 $EnergySavings_{Control} = 557038062$ **Btu**

 $EnergyCostSaved_{Control} = EnergySavings_{Control} \cdot FuelCost\$ = 7409 \$$ \$7,409

Install Blowdown Heat Recovery System:

<u>Existing Condition:</u> Currently the fuel oil from a back oil pressure control valve (back pressure) surplus oil not being used to the boiler burners goes through a blow down heat exchanger and then returns to the oil storage tanks.

<u>Proposed Modification:</u> All of the available blowdown heat is not being utilized in heating of the fuel oil being returned to the oil storage tanks. Also, this represents a risk of contaminating the fuel with water in the event the heat exchanger would leak. This proposal would be to remove the blowdown water to oil heat exchanger and install a new heat exchanger that would use the available heat in the blowdown water to preheat makeup water to the boiler.

% Flash Steam = ((SH-SL)/H)*100

SH=Sensible heat in the condensate at the higher pressure before discharge SL=Sensible heat in the condensate at the lower pressure to which discharge takes place H=Latent heat in the steam at the lower pressure to which the condensate is discharged Assuming the blowdown water is released to a flash steam system operating at 30 psig

$SH = 338 \frac{Btu}{lb}$	$SL \coloneqq 243 \cdot \frac{Btu}{lb}$	$H \coloneqq 929 \cdot \frac{Btu}{lb}$	
PercentFlashSteam	$\coloneqq \left(\frac{SH - SL}{H}\right) = 10.23\%$		
Energy in flash steam (E	EFS):		
$EFS \coloneqq PercentFlash$	$BSteam \cdot BD_{Prop} \cdot (H)$	<i>EFS</i> =69161	Btu hr



$EC \coloneqq BD_{Prom} \cdot (1 - PercentFlashSteam)$	$EC = 158815 \frac{Btu}{E}$
	hr
Energy Savings with blowdown heat exchar	nger efficiency of 95%:
$EnergySavings_{PDHP} \coloneqq \frac{EFS + (EC \cdot 0.98)}{EFS + (EC \cdot 0.98)}$	(5) HR EnergySavingspour = 2394419473 Btu
BE	
$EnergyCostSaved_{BDHR}{\coloneqq} EnergySaving$	hgs_{BDHR} • $FuelCost$
$EnergyCostSaved_{BDHB} = 31846$ \$	\$31,846

Water Conserved:

Tempering Water Saved:

Energy in condensate (EC):

To calculated the amount of tempering water saved we use the following relationship to solve for Mtempering, which is the flow of tempering water required in gpm, using the following relationship:

Tdrain * Mdrain = Ttempering * Mtempering + Tbddrain * Mbddrain

Mdrain = Mtempering + Mbddrain

Solving for Mtempering;

Mtempering = Mbddrain * (Tbddrain-Tdrain)/(Tdrain-Ttemp)

This is solved for the original blowdown case. Once the heat recovery unit is implemented, the heat exchanger drain temperature will be low enough so that tempering water is not required. Therefore, all current tempering water is saved.

$BD_{Exist} = 878.63 \frac{lb}{hr}$	$T_{BDExist} \coloneqq 212 \ ^{\circ}F = 671.67 \ R$
$M_{BDDrain} \coloneqq BD_{Exist} \cdot (1 - Percent)$	$FlashSteam) = 788.78 \frac{lb}{hr}$
$M_{tempering} \! \coloneqq \! M_{BDDrain} \! \cdot \! \left(\frac{\left(T_{BDExist} \right) \! \left(T_{SL} \! - \! T_{SL} \! - \! T_{SL} \right) \! \left(T_{SL} \! - \! T_{SL} \right) \! \left(T_{SL} \! - \! T_{SL} \!$	$\frac{-T_{SL}}{T_{MW}} = 631.02 \frac{lb}{hr}$



$$V_{tempering} \coloneqq M_{tempering} \frac{1}{8.34} \frac{gal}{lb} \frac{hr}{60 \min} = 1.26 \frac{gal}{\min}$$
$$V_{TempPerYear} \coloneqq V_{tempering} \cdot 60 \frac{\min}{hr} \cdot HR = 662802 \text{ gal}$$

Makeup Water Saved:

The amount of makeup water saved is equal to the reduction in blowdown flow plus the flash steam utilized with the new system.

$$\begin{split} M_{MUSaved} &\coloneqq BD_{Exist} - BD_{Prop} + BD_{Prop} \cdot \left(PercentFlashSteam\right) = 225.07 \frac{lb}{hr} \\ V_{MUSaved} &\coloneqq M_{MUSaved} \frac{1}{8.34} \frac{gal}{lb} \frac{hr}{60 \min} = 0.45 \frac{gal}{\min} \end{split}$$

$$V_{MUSavedPerYear} \coloneqq V_{MUSaved} \cdot 60 \frac{min}{hr} \cdot HR = 236403 \text{ gal}$$

 $WaterSaved \coloneqq V_{TempPerYear} + V_{MUSavedPerYear} = 899205 ~gal$

 $WaterCostSaved := WaterSaved \cdot Water\$ = 4496 \$$ \$4,496

Summary:

 $TotalCostSaved \coloneqq EnergyCostSaved_{Control} + EnergyCostSaved_{BDHR} \triangleleft = 43750 \ \$ + WaterCostSaved$

 $Total Energy Saved \coloneqq Energy Savings_{Control} + Energy Savings_{BDHR} = 2951457535 \ \textbf{Btu}$

 $FuelOilSaved := \frac{TotalEnergySaved}{FuelHV} = 19367$ gal

WaterSaved=899205 gal